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**DESIGN OF FENDER SYSTEM** 

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#### 1) HICOR Fender

The purpose of the fendering system is to serve as a bumper to protect the hull and berthing facility from damage when vessels berth alongside.

Another function is to operate as a shack absorber by absorbing the berthing energy of a vessel on the berthing operation and soften the berthing impact to the berth and hull.

Therefore, the two main functions of the fendering system are:

- To perform as a bumper to protect the hull and berthing facility from damages.
- To perform as a shock absorber on the berthing operation.

The adoption of a suitable fendering system will help to ensure smooth berthing operation.

Hence it is important to give priority to the selection of a fendering system that can actually

reduce the whole berthing facility construction cost, instead of simply choosing low-cost fenders.

#### 2) History

In the early days, vessels are made of wood and run by wind or human efforts. There was no necessity to use special fenders other than timber fenders for berthing vessels.

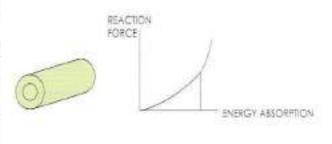
With the advanced technologies after the industrial revolution, vessels are propelled by steam engines or diesel engines, and hull are constructed out of steel in place of wood.

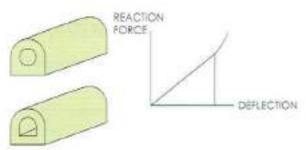
It becomes possible for larger size vessels to be onstructed with thinner and weaker hulls structures with improved knowledge in ship-building and cost minimization.

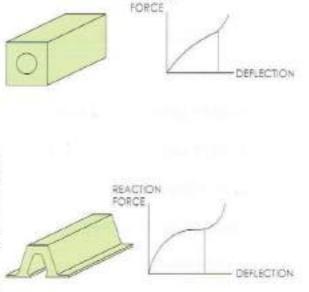
Due to the lack of suitable fendering system, large vessels were forced to moor at anchorages and cargoes were transferred by small boats or barges. Alternatively, the large vessels had to berth alongside with strong hull construction. With the development of mass transportation, it was important to develop fendering system to enable vessels to berth alongside of the quay.

Cylindrical type rubber fenders was developed in the 1940's, which allowed vessels to berth directly at the wharves. However the cylindrical fender is easily damaged because it is installed by chains and shackles, and has a high reaction force.

To overcome the above defects, V-shape fenders were developed after some research and development works done by the relevant authorities, together with fender manufacturing in Japan in the 1960's.







REACTION



V-shape fenders are anchored directly onto the quay walls instead of securing chains as in the case of cylindrical fenders. It offers better durabilities and energy absorption capacity with lower reaction force as compared with cylindrical fenders.

After 1960's, the research and development works continued to develop more ideal fenders for each individual special requirement.

Today, with the correct application of the suitable fendering systems from various kinds of fenders, construction costs of berthing are nationalized.

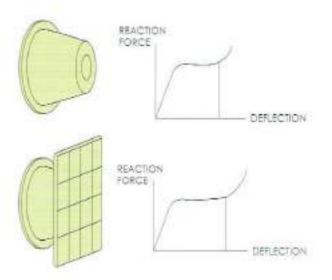
You can select suitable fenders to meet your requirements, for berthing of small boats to super tanker, from cylindrical type fenders.Vshape fenders, improved V-shape fenders, circle fenders, improved circle type fenders, fenders with steel frontal panels, pneumatic ar foam type floating fenders, tugboat fenders, roller fenders, and simple D or square shaped fenders.

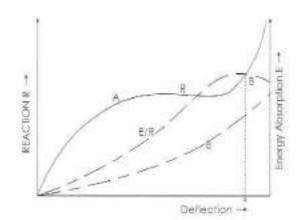
#### 3] FENDER TYPES AND CHARACTERISTICS

#### 3-1) Characteristics of fenders

The characteristics in terms of performance of rubber fenders are expressed by:

- A) Energy absorption: E (Tonf M) "Rated energy absorption" is the amount of energy absorbed by the fender when it is compressed to the rated deflection. It is given by area under the reaction deflection curve.
- B) Reaction force: R (Tant) "Rated reaction force" is the reaction force corresponds to rated deflection.
- C) Rated deflection: (%) "Rated deflection" is the most efficient on the relation between energy absorption value (E) and reaction load value (8, that is the deflection at which the ratio of E to R makes the maximum values (E/R).
- D) Hull pressure: (Tonf/m<sup>2</sup>) "Hull (surface) pressure" is the force transferred to hull (per sq. meter) of a ship fram the fender. Hull (surface) pressure = (reaction force)/ (contact area).









#### 3-2) Types of fenders

During compression for some fenders, the relationship between deflected in Fig. 1-1, while Fig.1-2 depicts the performance curve of the other fenders. [Deflection is expressed by a ratio to height of fender).

Buckling (Constant Reaction) type fenders having the performance curve as shown in Fig.1-1 will have a reaction load that suddenly rises comparatively as a result of elastic compressive deformation in the initial stage of deflection. However, when the reaction load reaches point A, it tends to remain almost constant within a certain zone regardless of increase in deflection once elastic buckling deformation has taken place. If the deflection progresses further, hollow section of fender will be closed and elastic compressive deformation will be restored resulting in a sudden rise in reaction load.

Fenders having the performance curve as shown in Fig.1-2 are the constant elastic modulus type fenders, and hallow cylindrical fenders will fall into this category. Approximately in proportion to increase in deflection, the reaction load will gradually increase and then suddenly rise after it reaches point 8 where the hollow section is closed. In this case, similar to bucking type fender. The deflection carresponds to paint B (see Fig.1-2 for the prescribed deflection).

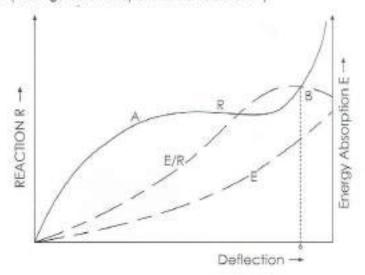


Fig.1-1 Performance Curve

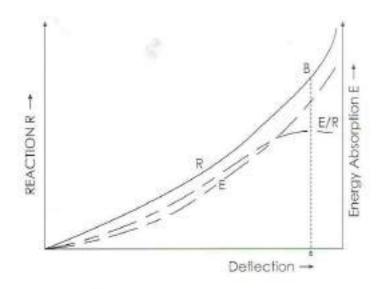


Fig.1-2 Performance Curve

#### DESIGN DATA COLLECTION



1] BASIC ITEMS FOR FENDER'S SELECTION

- A) Berthing energy
- B) Allowable reaction force from fender to the structure
- C) Allowable hull (surface) pressure
- D) Position and area to be protected by fendering system
- E) Natural force (wind, current, wave)
- 2] REQUIRED INFORMATION
- (\*: important)

#### 2-1) Vessels (refer to chapter 3.1): vessel

- A) Type \*
  - : General cargo, Oil tanker. Container carrier, Bulk carrier, Ferry boat, Passenger boat. Work boat, Tug boat, War ship.
- B) Weight\*
  - : D.W.T., D.P.T., or gross ton
- C) Length
- : Loa or Lpp
- D) Breadth
- E) Draft
- G) Free board

#### 2-2) Berthing facility (Berthing structure)

- Al Type\*
- : Wharf, Jetty, Pier, Dolphin or Pontoon
- B) Structure
- : Pile type or gravity type
- C) Elevation\*
- : Top deck (platform) level, High water and Low water level.
- For existing quay structure, the following additional information are required:
- D \* Space for fender installation with its elevations from sea water level.
- E] \* Horizontal allowable force acting on the structure.

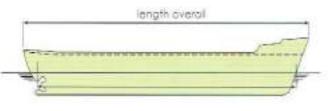
#### 2-3) Natural condition

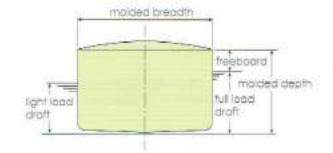
- A) Wind: Direction and speed
- B) Current: Direction and speed
- C) Wave: Height, period and direction



#### 1] VESSEL

As a general rule, one should use the actual values of the ship to calculate the berthing energy. However, in some cases where the actual values are not known, one can refer to the attached "Appendix C TableC-1" on Page 16 showing the typical ship's measurements given by the PIANC 2002\*.





Usually, ships are built according to the standard sets of dimensions and carrying capacity. The terminology used are defined as follows:

TERMINOLOGY		DEFINITIONS
Gross Tonnage	GT (ton)	Total volume of vessel and cargo. It is derived by dividing the total interior capacity of a vessel by 100 cubic feet.
Net tonnage	NT (ton)	Total volume of cargo that can be carried by the vessel.
Displacement Tanhage	DPT (ton)	Total weight of the vessel and cargo when the ship is loaded to draft line.
Dead Weight Tonnage	DWT (ton)	Weight of cargo, fuel, passenger, crew and food on the vessel.
Light Weight	LW (ton)	Weight of ship.
Ballast Weight	BW (toin)	Weight of ship and water added to the hold or ballast compartment of a vessel to improve its stability after it has discharged its cargo.
Length of ship	Loo or Lpp (m)	The length from the top of the bow to the end of the stern of a ship.
Breadth of ship	8 (m)	The distance across the parallel section of the sides of a ship.
Loaded Drafi	d (m)	The distance from the water surface to the keel of the ship when the ship is loaded to the freeboard mark.
Light Draft	db (m)	The distance from the water surface to the keel of the ship when the ship is at light.
Depth of Ship	D (m)	The octual Depth of ship.

Note: PIANC\* : PIANC Working Group MarCom WG33 Guidelines for the design of Fender Systems: 2002.



2) BERTHING ENERGY

#### 2-1) Berthing Energy

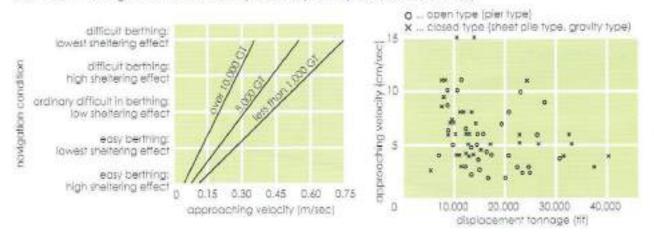
Effective berthing energy is calculated as follows:

$$E = \frac{M \cdot V^2}{2 \cdot g} Ce. Cm. Cs. Cc.$$

where:

E : Effective berthing energy (ton-m)

- M : Displacement tonnage (tans)
- V : Berthing velocity (m/sec)
- Ce : Eccentricity Coefficient
- Cm : Hydrodynamic Mass coefficient
- Cs : Softness coefficient (Generally accepted coefficient 1.0)
- Cc : Berth configuration coefficient (Generally accepted coefficient 1.0)



g : Acceleration of Gravity (9.8m/sec<sup>2</sup>)

#### 2-2) Berthing velocity (V)

Berthing velocity is one of the most important factors for designing a fendering system. Berthing velocity of vessels is determined from values of measure or from experience at existing berthing facility.

Generally, we would like to suggest following figures as designated berthing velocity.

- a) Good berthing conditions, sheltered.
- b) Difficult berthing conditions, sheltered.
- c) Easy berthing conditions, exposed.
- d) Good berthing conditions, exposed.
- e) Navigation conditions difficult, exposed.
- \* These figures should be used with caution as they are considered to be high.

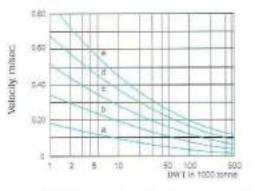


Figure 4.2.1. Design berthing velocity (mean value) as function of navigation conditions and size of vessel (Brotsmallet al. 1997)



#### 2-3) Hydrodynamic Mass coefficient: Cm

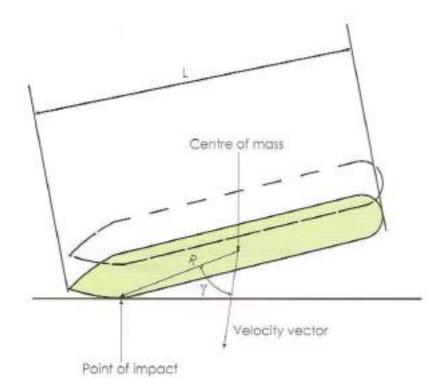
The hydrodynamic mass coefficient allows the movement of water around the ship to be taken in account when calculating the total energy of the vessel by increasing the mass of the system. The hydrodynamic mass coefficient (Cm) may be calculated by the following equation.

CM = 1 + (2d/B)

#### 2-4) Eccentricity coefficient: Ce

A ship mostly berths at a certain angle. Therefore, vessel turns simultaneously at the time offirst contact. Some of the kinetic energy of the ship is converted to turning energy, and the remaining energy is transferred to the berth. The eccentricity factor (Ce) represents the proportion of the remaining energy to the kinetic energy of the vessel at berthing.

 $Ce = (K^2 + R^2 X \cos^2 \gamma) / (K^2 + R^2)$ 



- K = radius of gyration of the vessel (depending on block coefficient, see below) (in m)
- R = distance of point of contact to the centre of the mass (measured parallel to the wharf) (in m)
- y = angle between velocity vector and the line between the point of contact and the centre of mass.



### $K = (0.19 \text{ Cb} + 0.11)^* \text{Lpp and } \text{Cb}_* \frac{M}{L^* B^* D^* p}$

Where:

Cb = block coefficient (usually between 0.5 - 0.9, see below)

M = mass of the vessel (displacement in tannes);

- L = length of vessel (in m):
- B = breadth of vessel (in m):
- D = draft of vessel (in m);
- density of water (about 1.025 ton/m<sup>2</sup> for sea water)

Lacking other data, the following may be adopted for the black coefficient

For container vessels	0.6 - 0.8		
For general cargo vessels and bulk carriers	0.72-0.85		
For tankers	0,85		
For ferries	0.55-0.65		
For Ro/Ro-vessels	0.7 - 0.8		

#### 2-5) Soffness Coefficient (Cs)

Part of the kinetic energy of the berthing vessel will be absorbed by elastic deformation of the vessel hull.

Cs is generally taken as 1.0

Cs for VLCC is used as 0.9

#### 2-6) Berth Configuration Coefficient (Cc)

The berth configuration coefficient ("Cushion Factor") indicates the difference between an open structure (e.g. piled [etty] and closed structure (e.g. quay wall)

For open berth and corners of quay wall Cc is generally taken as 1.0

For (solid) quay wall under parallel approach Cc is generally taken as 0.9

#### 2-7) Abnormal Impact

Fenders have to be capable at catering for a reasonable abnormal impact. The following table gives general guidance on the selection of the factor for abnormal impact to be applied to the design energy.

The factor of abnormal impact should not be less than 1.1

Type Of Berth Impoct	Vessel	Factor for Abnormal Impact Applied to Berthing Energy (Cab)
Tanker and Bulk Cargo	Lorgest Smallest	1.25 1.75
Container	Largest Smallest	1,5 2.0
General Cargo Ro-Ro and Ferries		1.75 2,0 or higher
Tugs, Work Boats, etc.		2.0



#### 3) ALLOWABLE REACTION FORCE

The allowable reaction force from the impact of the ship is governed by the designed lateral resistance of the berthing structure. If the lateral resistance is exceeded, the structure would be damaged. (This reaction force would also act on the hull of the berthing ship. If the pressure exceeds the hull resistance, the hull would be damaged.) Therefore the fendering system must be designed such that

#### REACTION FORCE IN FENDERS < LATERAL RESISTANCE OF STRUCTURE

It is important to note that the reaction force from the impact of a ship is not a constant value. It varies with deformation and is represented by the performance curves of the protecting fender. In design, different types and combination of fenders may be fired out, so as to arrive at a rated reaction force below the allowable resistance of the berthing structure. Generally, the lateral resistance of dolphins and open piled piers are lower than that of the more massive quay wall structures.

#### 4) ALLOWABLE HULL (SURFACE) PRESSURE

#### 4-1) Allowable hull (surface) pressure

The data is not available. In the design of fenders for dangerous cargo vessel such as all tanker, Allowable hull pressure ranges from 20 tons/m².

There, however, are many cases of tankers berthing on to the fender with surface pressure exceeding 100 tons/m<sup>2</sup> without any damage of the hull

Type Of Vessel	Hull Pressure kN/m <sup>2</sup>		
Container vessels 1st and 2nd generation	< 400		
3rd Generation (Panamax)	< 300		
4th Generation	<250		
5th & 6th Generation	<200		
General Cargo Vessels			
=/< 20.000 DWT	400 - 700		
> 20.000 DWT 40	<400		
Oil Tanker			
#/< 60.000 DWT	< 300		
> 60.000 DWT	< 350		
VLCC	150 - 200		
Gas Carries (LNG / LPG)	< 200		
Bulk Carries	< 200		
SWATH			
RO - RO Vessel	These vessels are usually belter		
Passenger Vessel			

#### 4-2) Actual values of typical fender

 The following are the surface pressure of typical fender:

 V-Shape
 : 50 - 140 (ton/m²)

 Improved V-shape
 : 40 - 120

 Floating type fender
 : 10 - 25

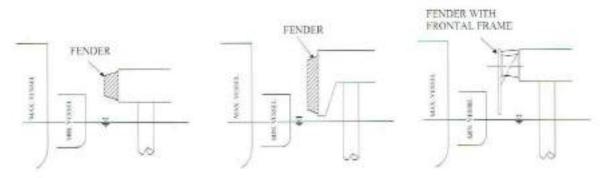
 Fender with frontal panel
 : values can be adjusted by changing the size of the frontal panel



#### 5) POSITION AND AREAS TO BE PROTECTED

#### 5-1) Vertical Direction

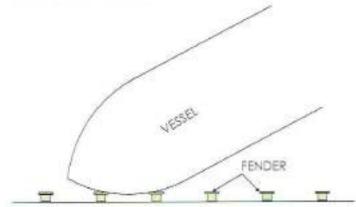
The types of the fenders and its position at the quay must be determined to protect and absorb the berthing energy of all types and size of vessels at all possible tidal range.



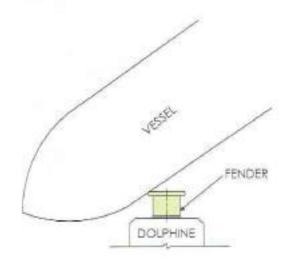
#### 5-2) Horizontal Direction

The interval of the fenders must be determined so as to avoid direct contact with the quay wall under the designed berthing angle and designed deflection of the fenders.

- 1) Continuous Wharf
- (\* Refer to ITEM 7) " FITTING INTERVAL OF FENDER"



2] Dolphins Wharf





#### 6) NATURAL FORCE

#### 6-1) Wind Force

The wind force acting on the ship in moorage shall be determined using an appropriate method of Calculation. In general, the wind pressure is calculated by the following formula (refer to FIG. 3-10)

 $R1 = \frac{1}{2} \rho \cdot C \cdot U^{2} (A_{1} \cdot \cos^{2}\theta + A_{1} \cdot \sin^{2}\theta)$ 

where ;

- R1 : Resultant force of wind pressure (kg)
- P : Air density (= 0.123kgs²/m²)
- U : Wind speed (m/s)
- A. : Area of projection of the front of ship above water surface (m<sup>2</sup>)
- A<sub>11</sub>: Area of projection of the side of ship above water surface (m<sup>2</sup>)
- 8 ; Angle of the wind direction to the center line of the hull (deg)
- C : Coefficient of wind pressure

General Cargo: C = 1.325 - 0.05cos26 - 0.35cos49 - 0.175cos68

Passenger Ship: C = 1.142 - 0.142cos29 - 0.367cos49 - 0.133cos69

Oil Tanker C = 1.20 - 0.083cos20 - 0.25cos40 - 0.177cos60

#### 6-2) Current Force

The resultant force due to the current in the direction of the ship side is calculated by the following formula:

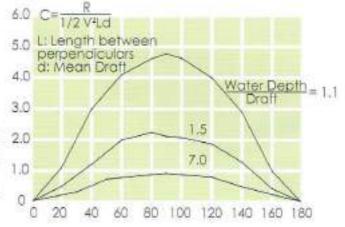
 $R2 = 0.5 * p * C * V^2 * As^2$ 

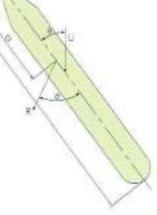
Where ;

- R2 : Resultant force due to the current (kgf)
- P : Seawater density (= 1.025ton/m3)
- C : Coefficient of fluid pressure
- V : Current speed (m/s)
- As<sup>2</sup> : Area of ship side below the draft line (m<sup>2</sup>)

#### 6-3) Wave Force

The wave forces acting on the mooring ship can be calculated by appropriate methods such as the source method, the boundary element method, the finite element method, and the strip method which is most widely used for ships.







7) FENDER SPACING

A ship berths at a certain angle and contacts with the berth at certain point of bow or stern of the ship.

The fitting fender spacing should be determined at a point where ships do not crosh during berthing.

At a suitable spacing, the following table is introduced in Technical Note No.30, Japan.

Water Depth	Fender Spacing
-46m	4 <del>-</del> 7m
-6 – -8m	7 – 10m
-8 ~ -10m	10 - 15m

The following equation can be used for determining the maximum fender spacing.

 $L = 2\sqrt{r^2 - (r - h)^2}$ 

where ;

L : maximum fender spacing (m)

r : bent radius of bow side of ship (m)

h : Height of fenders when effective berthing energy absorbed (m)

If the information of a bent radius of board side is not available, then following equations offer a guideline to the bent radius.

General Carao --500 DWT - 30,000 DWT

Bow 5°: log r = -0.853 + 0.640 log (DWT) 10°: log r = -1.055 + 0.650 log (DWT)

140	30,000	) DW	r~	
P	Lpp <sup>2</sup>		В	
H-	168	<b>T</b>	4	

Tanker, Ore Carrier ----DWT 5.000 DWT ~ 30.000 DWT

Bow 5° : log r = - 0.541 + 0.560 log (DWT) 100 : log r = - 0.113 + 0.440 log (DWT) \* (DWT): Dead weight Tonnage of Vessel

θ

30,000 DWT ~	
--------------	--

On La	30,000 DWT ~				
8-	Lpp <sup>2</sup>		В		
<i>n</i> -	16B	*	4		



#### 8) DESIGN EXAMPLES

#### (1) Example 1

#### i) Design Vessel

Vessel Type	General Cargo			
DWT (tons)	15,000	1,000		
Loa (m)	156	67		
Lpp (m)	147	62		
B (m)	23	10.8		
D (m)	13.1	5,8		
d (m)	10.4	3.9		
V (m/sec)	0.15	0.25		
Berthing Point	1/4 point	1/4 point		
Eccentricity Coefficient	0.5	0.5		

#### II) Facility

Wharf Length	: 180 meter
	continuous face
H.W.L.	: + 2.0m
L.W.L	: + 0.3m
Top elevation of deck	: + 3.0m

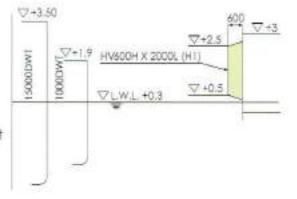
#### ili) Berthing energy

DWT (ton)	Ws (ton)	Cb	Cm	Ce	V (m/sec)	B/E (tonf-m)
15.000	21,600	0.599	1.834	0.5	0.15	22.7
1,000	1,690	0.631	1.808	0.5	0.25	4.9

#### iv) Selection of fender

HV type fender model	:HV600H x 2000L [HI]
Performance Fender Heig	ght : 0.600 meter
Rated Deflection	: 52.5%
Reaction Force	: 99.5 Tonf
Energy Absorption	: 25.1 Tonf-m > 22.7 Tonf-m
Surface Pressure	: 73.7 Tonf/m <sup>2</sup>

Relation of fenders & vessels at L.W.L. In the case of 1.000 DWT's berthing at L.W.L., the contact length of vessel to fender is 1.4 meter [= 1.9 - 0.5]. The energy absorption of 1.4 meter length of fender is: 17.6 Tonf-m/1.4 m > 4.9 Tonf-m.





#### v) Fender Spacing

Please refer to data below for maximum spacing.

Vessel	4	-	15,000 DWT	1.000 DWT
Bent Radius	1	r (m)	45	8
Fender Height	14	H (m)	0.6	0.6
Fender Deflection	4	d (m)	0.315	0.138
			(52.5%)	[23%]
Deflected Fender Height	- 3	h (m)	0.285	0.462
Max Spacing	-1	L (m)	10.1	5.3

We would recommend 5.0 meters of fender spacing as to accommodate the minimum vessel for 1,000 DWT

#### (2) Example 2

#### i) Vessel

Kind	Ore Carrier	General Cargo		
DWT (tons)	40,000	2,000		
Loa (m)	194	83		
Lop (m)	182	77		
8 (m)	28.4	13.1		
D (m)	15.8	7.2		
d (m)	31.4	4.9		
V (m/sec)	0.12	0.20		
Berthing Point	1/4 point	1/4 paint		
Eccentricity Coefficient	0.5	0.5		

#### ii) Facility

 Wharf Length
 : 250 meter continuous face

 H.W.L.
 : + 3.5 m

 L.W.L
 : + 0.3 m

 Top elevation of deck
 : + 4.5 m

 Battom elevation of deck
 : + 2.5 m

#### iii) Berthing energy

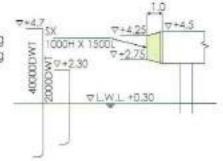
DWT (ton)	Ws (ton)	Cb	Cm	Ce	V (m/sec)	B/E (tonf-m)
40,000	48.586	0.804	1.803	0.5	0.12	32.2
2.000	3.250	0.641	1.772	0.5	0.2	5.9



#### iv) Selection of fender

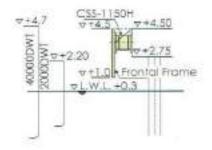
#### = Wrong Selection =

If we select the fender only basing on the calculated berthing energy 32.2 Tonf-m and given space for fender installation, following SH-Fender can be selected as one of the fenders to be installed. Type of fender : \$X1000H x 1500L (H3) Performance Rated Deflection : \$2.5% Reaction Force : 82.9 Tonf Energy Absorption : 34.8 Tonf-m > 32.2 Tonf-m Surface Pressure : 49 Tonf/m<sup>2</sup>

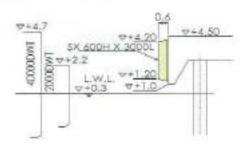


From the above, the small vessel, 2,000 DWT has no contact with the fender. Therefore, the selected fender is not suitable for this application.

Performance Rated Deflection	: C5S-1150H (F2) : 52.5% : 76.3 Tonf : 38.6 Tonf-m > 32.2 Tonf-m : 1.75 mW x 3.5 mL
------------------------------	---



= Good Selection = Alternative 2	
	: SX 600H x 3000L (H1)
Performance Rated Deflection	: 52.5%
	: 149 Tonf
Energy Absorption	: 37.6 Tonf-m > 32.2 Tonf-m
Surface Pressure	: 74 Tonf/m²





#### STANDARD SIZE OF VESSELS

	Deed	Displa-	Length	Length	Breadth	Depth	Maximum	Wind Lat	dence Limit. eret áree	75% Wint Fr	ant Arias
Туре	Weight	cement	0.000	1.	Street in	Sebui		Sector Las	Codi re pa		Conc. Contra
	Tonnage	Constant-	Qverall	P.P.			Draft				
	(1)	(1)	(m)	(m)	(m)	(m)	(m)	(17	100 C	1.	n?)
								Full Load Condition	Ballest Condition	Full Load Condition	Ballast Condition
General	1,000	1,690	67	62	10.5	臣臣	3.9	278	342	63	93
Cargo	2.000	3.250	83	77	13.1	7.2	4,9	428	541	101	142
Ship	3,000	4,750	95	88	14.7	8,1	5.6	547	708	132	182
	5,000	7,890	111	104	18.9 18.6	9,4	6.6	750	993 1,240	185	249 307
	7,000	10,500	123 137	115 129	20.5	10,4 11.6	7.4	1,150	1,570	294	382
	15,000	21,600	155	147	23.0	13,1	9.5	1,480	2,080	385	490
	20,000	28,400	170	161	24.9	14.3	10.4	1,760	2,790	466	585
	30,000	41,500	193	183	27.8	18.2	†1.9	2.260	3,250	B11	750
	40,000	54,500	211	200	30.2	17.6	13.0	2,700	3,940	740	895
Buk	5,000	6,920	109	101	15.5	8.6	6,2	669	910	221	245
Carner*	7,000	9,520	120	111	17.2	9.5	6.9	795	1,090	250 286	287
	10,000	13,300 19,600	132 149	124 140	19.2 21.8	10.6 11.9	7.7	930	1,320	332	340 411
	20,000	26.700	181	152	23.8	13.0	9.4	1,240	1,900	389	470
	30,000	37,700	181	172	27.0	14.7	10.街	1,480	2,360	428	569
	50,000	61,100	209	200	32.3	17.1	12.4	1,830	3,090	518	723
	70,000	84,000	231	221	32.3	18.9	13.7	2,110	3,690	555	846
	100,000	118,000	255	246	39.2	21.1	15.2	2,480	4,460	669	1,000
	150,000	173,000	267	278	44.5	23.8	17.1	2,920	5,520	777	1,210
	200,000 250,000	227.000 280,000	311 332	303 324	48.7 52.2	25.9 27.7	18.8 19.9	3,300 3,630	6,430 7,240	884 938	1,380
Container	7,000	10.700	123	115	20.3	9.8	7.2	1,480	1,590	330	444
Ship**	10.000	15,100	141	+32	22.4	11.3	8.0	1,880	1,990	410	535
	15,000	22.200	166	166	26.0	13.3	9.0	2,490	2,560	524	663
	20,000	29,200	186	175	27.1	14,9	9.9	3,050	3,070	625	771
	25,000	36,100	203	191	28.8	16.3 17.5	10.5	3,570	3,520 3,950	716	870 850
	30,000 40,000	43.000 56,500	218 244	205 231	30.2 32.3	19.8	12.2	4,970	4,730	950	1,110
	50,000	89,900	266	252	32.3	21.4	13.0	5.810	5,430	1.090	1,250
	60,000	83,200	285	271	36.5	23.0	13.8	6,610	6,090	1,220	1.370
Qil	1,000	1,560	61	58	10.2	4.5	4.0	190	280	86	85
Tanker	2.000	3,070	76	72	12.8	5.7	4.9	280	422	119	125
	3,000	4,520	87	82	14.3	6.6	5.6	351	536	144 184	156 207
	5,000	7,360 10,200	102	97 108	16.6 15.6	7.9 8.9	6.4 7.1	467	726 885	216	249
	10,000	14,200	127	121	20.8	10.0	7.9	658	1.090	255	303
	15,000	21,000	144	138	23.6	11.6	8.9	860	1,390	309	378
	20,000	27,700	158	151	25.8	12.8	9.6	1.010	1,850	355	443
	30,000	40,800	180	173	29.2	14.8	10.9	1,270	2,090	430	564
	50,000	66,400	211	204	32.3	17.8	12.8	1,690	2,830	548	734
	70.000	91,600	235	227	38.0	19.9	13.9	2,040	3,460	642	884
	100.000	129.000	263	254	42.6	22.6	15,4	2,490	4,270	761	1,080
	150.000	190.000	298	290	48,1	25.9 28.7	17.4	3,120 3,670	5,430 6,430	520	1,340
	200,000	250,000	327	318	52.6						1,970
	300.000	366.000	371	363	59.7	33.1	21.2	4,600	8,180	1,280	

\*Excerpt from "PIANC Working Group MarCom WG33 Guidelines for the design of Fender Systems: 2002"



Appendix (	2. Table C-1						1000		dence Limit		
Туре	Deed Weight Tonnege	Displa- cement	Length Overali	Length P.P.	Breadth	Depth	Meximum Draft	Wind Lai	eral Aree	Wind Fr	ont Area
	(t)	(1)	(m)	(m)	(m)	(m)	(m)	(m <sup>a</sup> )		10	18)
				1000				Full Load Condition	Balast	Full Load Condition	Ballast
Ro/Ro	1,000	2,190	73	66	14.0	6.2	3.5	880	970	232	232
Ship	2,000	4,150	94	86	16,6	8.4	4.5	1,210	1,320	314	325
	3,000	6,030	109	99	18.3	10.0	5.3	1,460	1,590	374	391
	5,000	9,670	131	120	20.7	12.5	6.4	1,850	2,010	467	497
	7,000	13,200	148	136	22.5	14.5	7.2	2,170	2,350	541	583
	10,000	18,300	169	155	24.6	17.0	8.2	2,560	2,760	632	690
	15.000	26,700	196	180	27.2	20.3	9.6	3,090	3,320	754	836
	28,000	34,800	218	201	29.1	23.1	10.7	3,530	3,780	854	960
	30,000	50,600	252	233	32.2	27.6	12.4	4,260	4,550	1,020	1,160
Passenger	1,000	1,030	.64	60	12.1	4,9	2.6	464	486	187	197
Ship	2,000	1,910	81	76	14.4	6.3	3.4	744	770	251	283
	3,000	2,740	93	86	15.0	7.4	4.0	980	1,010	298	311
	5.000	4,320	112	102	18.2	9.0	4.8	1,390	1,420	371	385
	7,000	5,830	125	114	19.8	10,2	5.5	1,740	1,780	428	444
	10,000	8,010	142	128	21.6	11.7	6.4	2,220	2,250	498	516
	15,000	11,500	163	146	23.9	13.7	7.5	2,930	2,950	592	611
	20,000	14,900	180	160	25.7	15.3	8.0	3,560	3.570	669	690
	30,000	21,300	207	183	28,4	17.8	8.0	4,690	4.680	705	818
	50,000	33,600	248	217	32.3	21.7	8.0	6,640	6,580	990	1,010
	70,000	45.300	278	243	35.2	24.6	8.0	8,350	8,230	1,140	1,170
Ferry	1,000	1.230	67	.61	14,3	5.5	3.4	411	428	154	158
	2,000	2,430	88	78	17.0	6.8	4.2	656	685	214	221
	3,000	3,620	.89	91	18.8	7.7	4.8	862	903	259	269
	5,009	5,970	119	110	21.4	9.0	5,5	1,220	1,280	330	344
	7,000	8,310	134	124	23.2	10.0	6,1	1,530	1,600	387	405
	10,000	11,800	153	142	25.4	11.3	6.8	1,940	2,040	458	482
	15,000	17,500	177	164	28.1	12.6	7,6	2,550	2,690	555	586
	20,000	23,300	196	183	30.2	13.8	8.3	3,100	3,270	636	673
	30,000	34,600	227	212	33,4	15.8	9.4	4,070	4,310	771	819
	40.000	45,900	252	236	35.9	17.1	10.2	4,950	5,240	880	940
Gas	1,000	2,450	71	66	11,7	-5.7	4.6	390	465	133	150
Carrier	2,000	4,560	88	82	14.3	7.2	5.7	597	707	195	219
	3,000	6,530	100	83-	16.1	8.4	6.4	765	903	244	273
	5,000	10.200	117	109	18.8	10.0	7.4	1,050	1,230	323	361
	7,000	13,800	129	121	20.8	11.3	8.t	1,290	1,510	389	434
	10,000	18,900	144	136	23,1	12.9	9.0	1,800	1,870	474	527
	15,000	27,000	164	154	26.0	14.9	10.1	2,050	2,390	593	658
	20,000	34,800	170	169	28.4	16,5	11.0	2,450	2,840	698	770
	30,000	49,700	203	192	32.0	19,0	12.3	3,140	3,630	870	961
	50,000	78,000	237	226	37.2	22.8	12,3	4,290	4,940	1,150	1.270
	70,000	105,000	263	251	41.2	25.7	12.3	5,270	6,060	1,390	1,530
	100,000	144,000	294	281	45.B	29.2	12.3	6,568	7,510	1,690	1.880

\*) Full Load Condition of Wind Lateral / Front Areas of log carrier don't include the areas of logs on deck. \*\*) Full Load Condition of Wind Lateral / Front Areas of Container Ships include the areas of containers on deck.

"Excerpt from "PIANC Working Group MarCom WG33 Guidelines for the design of Fender Systems: 2002"

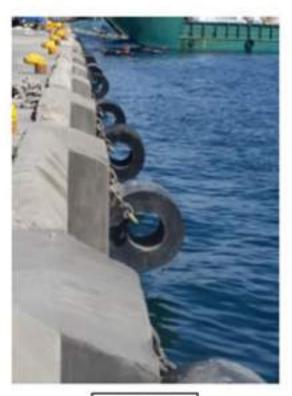


Туре	Dead Weight Tonnage		Xisplacemen (t)		50%, 75%, 95% Туре	Dead Weight Tonnage (t)	t	)isplacemen (t)	t,
	(1)	50%	75%	95%			50%	75%	1955
	1.000	100010			10.0	1.000			
General	1,000	1,850	1.690	1,850	RoRo	1.000	1,970	2,170	2,540
Cargo	2,000	3,040	3,250	3,560		2,000	3,730	4,160	4,820
Ship	3,000	4,460	4,750	5,210		3,000	5,430	6,030	7,010
	5,000	7,210	7,690	B,440		5,000	8,710	9.670	11,200
	7,000	9,900	10,600	11,600		7.000	11,900	13,200	15,300
	10,000	13,900	14,800	16,200		10,000	16,500	18,300	21,300
	15,000	20,300	21.600	23,700		15,000	24,000	2,705	31,000
	20,000	26,500	28,400	31,000		20,000	31,300	34,800	41,400
	30,000	39,000	41,600	45,800		36.000	45,600	50,600	58,800
	40,000	51,100	54,500	59,800					
					Passenger	1,000	-850	1,030	1,350
Bulk	5,000	6.740	6.920	7,190		2,000	1,580	1,910	2,500
Camer	7,000	9,270	9,520	9,880		3,000	2,270	2,740	3,59
	10,000	13,000	13,300	13,800		5,000	3,580	4,320	5,650
	15.000	19,100	19.600	20,300		7.0011	4,830	5,830	7,630
	20.000	25,000	25,700	26,700		10.000	6.640	8,010	10,500
	30,000	36,700	37,700	39,100		15,000	9,630	11,600	15,000
	50,000	59,600	61,100	63,500		20.000	12,300	14,900	19,400
	70.000	81,900	84,000	87,200		30,000	17,700	21,300	27,900
	100.000	115,000	118,000	122,000		50,000	27,900	33,600	44,000
	150,000	168,000	173,000	179,000		70,000	37,600	45,300	59,300
	200,000	221,000	227.000	236,000					
	250,000	273,000	280.000	291.000	Ferry	1.000	810	1,230	2,240
_						2,000	1,600	2,430	4,430
Container	7,000	10,200	10,700	11,500	1	5,000	2.390	3,820	6,990
Ship	10,000	14,300	15,100	18,200		5,000	3,940	5,970	10,900
	15,000	21,100	22.200	23,900		7.000	6,480	8,310	15,100
	20,000	27,800	29,200	31,400		10.000	7,770	11,800	21.500
	25,000	34,300	35,100	38,800		15.000	11,600	17,500	31,900
	30,000	10.800	43,000	46,200		20.000	15,300	23,300	42,300
	40,000	53,700	56,500	60,800		30,000	22,800	34,600	63,000
	50,000	66,500	69,900	75,200		40.000	30,300	45,900	83,500
	80,000	79,100	83.200	89,400					
00	1,000	1,450	1,580	1,800	Gas	1,000.0	2,210.0	2,480	2,910
Tanker	2.000	2.810	3.070	3,480	Çemier	2,000	4,080	4,560	5,37
	3.000	4,140	4,520	5,130	100	3.000	5.830	8,530	7,68
	5,000	6,740	7,360	8,360		5,000	9,100	10,200	12,000
	7,000	9,300	10.200	11,500		7.000	12,300	13,800	16,200
	10,000	13,100	14,300	16,200		10,000	18,900	18,900	22,200
	15,000	19,200	21,000	23,900		16,000	24,100	27,000	31,700
	20,000	25,300	27,700	31,400		20.000	31.100	34,800	40,900
	30,000	37,300	40,800	48,300		30,000	44,400	49,700	58,500
	50,000	60,800	85,400	75,500		50,000	69.700	78.000	91,600
	70,000	83,900	91,600	104,000		70,000	94,000	105,000	124,000
	100,000	118,000	129,000	148,000		100.000	128.000	144,000	169.000
	150,000	174,000	190,000	216,000					
	200.000	229,000	250.000	284,000					
	300,000	337,000	368,000	418,000					

\*Excerpt from "PIANC Working Group MarCom WG33 Guidelines for the design of Fender Systems: 2002"







BOHOL

# HICOR CELL TYPE FENDER



#### Introduction

In recent years while the economic blocks have expanded increasingly wider, the maritime distribution industry has entered into the era of high-speed distribution in large quantities, in which large-scale container ships are taking the initiative. Accordingly, the development and production of larger and faster vessels has raised the demand for lighter weight of the hull structure. This has also affected how a fender should serve as a crucial supporter in ensuring safe maorings of ships; as a result, the main stream has been shifting from the conventional types of fenders to the ones with higher absorbed energy and with lower reaction force. These allow less shock to be transmitted to the auter plank of the hull.

Conventionally, fender materials have been selected with priority given to whether or not they have sufficient ability to absorb the energy coming from a mooring ship. With progressing competition among harbor operators, however, there has been a growing tendency to place more priority over the cause no damage to the hull structure.

In particular, to select fenders intended for large scale container ships, considerations such as a "allowable hull pressure", "flexibility to widely-opened flare of the" or "easier maintenance check to important in addition to the conventional requirements" absorption of the berthing energy", relation between the pier strength and the fender's reaction force" and "durability of the fender". The "Circle Fender with Frontal Panel" is furnished with frontal frame whose front surface is covered with the resin sheet that allows a low co-efficient of friction. For a permissible surface pressure of the hull structure, surface reaction force of the fender (ton/m) can be adjusted simply by regulating the size of the frontal panel. For "flexibility to a flare angle of the hull", it employs a structure that enables the generated load to be received on its flat portions. The Circle Fender with Frontal Panel, whose rubber structure has no direct will suffer from rubbings or flaws. This fender which is designed appropriately, can give excellent durability to allow a service life of about 15 years only by applying a simple and easy maintenance check on the product.









TOLEDO POWER PLANT JETTY, TOLEDO CITY, CEBU HICOR CELL TYPE FENDER





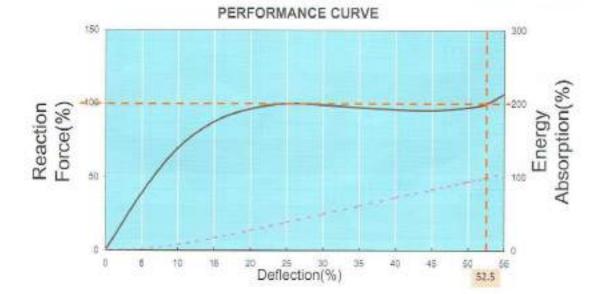


TOLEDO POWER PLANT JETTY, TOLEDO CITY, CEBU HICOR CELL TYPE FENDER

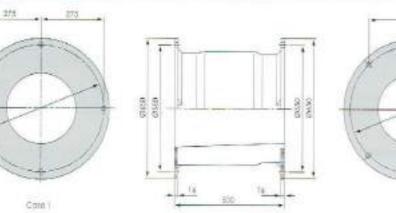


#### Velocity Factor

CSS.	0.1m/	sec VF	0,12m	(sec) VF	0.2m/	sec VF	0.25m/	sec VF	0.3m/	sec VF	-
0.33	R/F	E/A	R/F	E/A	R/P	E/A	R/F	E/A	R/F	E/A	CSS
400	0.968	0.967	0.983	0.982	1,023	1,024	1.040	1.042	1.055	1.057	400
500	0.968	0.966	0.982	0.981	1.023	1.024	1.041	1.043	1.055	1.055	500
600	0.965	0.966	0,982	0,981	1.023	1.024	1.041	1.043	1.056	1.039	600
800	0.967	0.965	0,982	0.981	1.024	1.025	1.042	1.044	1.057	1.060	800
1000	0.967	0,965	0,982	0.981	1,024	1.025	1.043	1.045	1.058	1.061	1000
1150	0.967	0.965	0.982	0.981	1.024	1.025	1.043	1,045	1.058	1.061	1150
1250	0.967	0.965	0.982	0.980	1.024	1.025	1.043	1.045	1.058	1.062	1250
1450	0.967	0.964	0.981	0.980	1.024	1.026	1.043	1.046	1.059	1.062	1450
1600	0.966	0.964	0.981	0.980	1.024	1.026	1.043	1.046	1,059	1.062	1600
1700	0,965	0.964	0.981	0.980	1.024	1.026	1.043	1.046	1.059	1.063	1,700
1800	0.966	0.964	0.981	0.980	1.024	1.026	1.044	1.046	1,059	1.063	1800
2000	0.966	0.964	0.981	0.980	1.024	1,026	1.044	047	1.060	1:063	2000
2250	0.966	0.963	0.981	0.980	1.025	1,026	1,044	1.047	1.060	1.064	2250
2500	0.966	0.963	0.981	0.980	1,025	1.026	1.044	1.047	060	1.064	2500
3000	D.966	0.963	0.981	0.980	1.025	1.027	1,044	1.048	1.060	1.065	3000







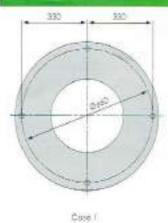
Core 1

194

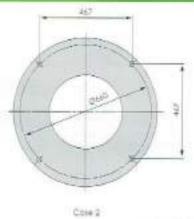
Weight Hold

	500H	F4	F3	F2	F1	FO
6	E/A(kN-m)	17.9	21.4	25.5	30.5	36.4
8	R/F(kN)	78.3	93.5	.111	133	159
14	E/A(kN-m)	18.5	22.0	26.3	31.4	37.5
	R/F(kN)	80.6	96.3	115	137	163
2	E/A(kN-m)	19.0	22.7	27.1	32.3	38.6
4	R/F(kN)	83.0	99.2	118	141	168
	E/A(kN-m)	19.6	23.4	27.9	33.3	39.7
3	R/F(kN)	85.5	102	122	145	173
	E/A(kN-m)	20.2	24.1	28.7	34.3	40.9
-9	R/F(KN)	88.1	105	125	150	179
5	E/A(kN-m)	20.8	24.8	29.6	35.3	45.0
9	R/F(kN)	90.7	108	129	154	197
Boll S	ize: X4pcs	M20	M20	M20	M20	M22

600H





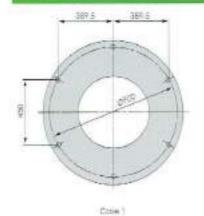


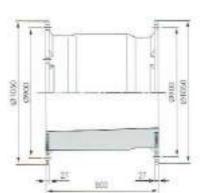
weight: 200kg

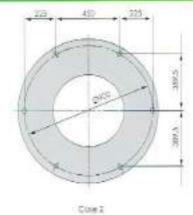
	600H	F4	F3	F2	F1	FO
	E/A(kN-m)	30.9	36.9	44.0	52.6	62.8
22	R/F(kN)	112	134	160	192	229
54	E/A(kN-m)	31.8	38.0	45.4	54.2	64.7
1	R/F(kN)	116	138	165	197	236
2	E/A(kN-m)	32.8	39.1	46.7	55.8	66.6
4	R/F(kN)	119	142	170	203	243
3	E/A(kN-m)	33.8	40.3	48.1	57.5	68.6
0	R/F(kN)	123	147	175	209	250
-	E/A(kN-m)	34.8	41.5	49.6	59.2	70.7
	R/F(kN]	126	151	180	216	258
5	E/A[kN-m]	35.8	42.8	51.1	61.0	77.7
3	R/F(kN)	130	156	186	222	283
Bolt S	ize: X4pcs	M22	M22	M22	M24	M24



800H



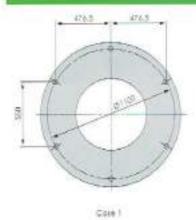


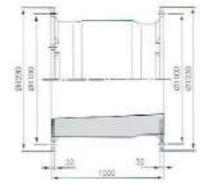


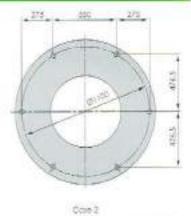
weight #25ig

	800H	F4	F3	F2	F1	FD
	E/A(kN-m)	73.1	87.3	105	125	149
0	R/F(kN)	200	239	285	341	407
Carlo -	E/A(kN-m)	75.3	89.9	108	129	153
1	R/F(kN)	206	246	294	351	419
18	E/A(kN-m)	77.6	92.6	111	132	158
2	R/F(kN)	212	253	303	362	432
245	E/A(kN-m)	79.9	95.4	114	136	163
3	R/F(kN)	219	261	312	372	445
145	E/A(kN-m)	82.3	98.3	118	141	168
4	R/F(kN)	225	269	321	384	458
16	E/A(kN-m)	84.8	102	121	145	184
5	R/F(kN)	232	277	331	395	504
Bolt S	ize: X6pcs	M22	M22	M22	M24	M24

1000H



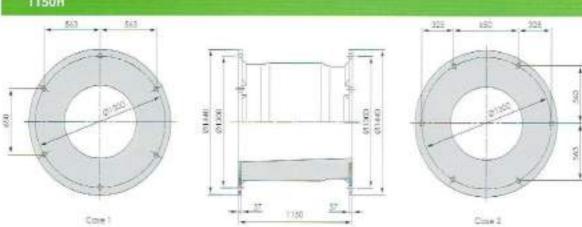




Weight 760kg

	1000H	F4	F3	F2	E1	FD
0	E/A(kN-m)	143	171	204	243	290
0	R/F[kN]	313	374	446	533	636
1	E/A(kN-m)	147	176	210	251	299
	R/F(kN)	322	385	460	549	655
	E/A(kN-m)	152	181	216	258	308
2	R/F(kN)	332	396	473	565	675
3	E/A(kN-m)	156	187	223	266	317
	R/F(kN)	342	408	488	582	695
12	E/A(kN-m)	161	192	229	274	327
4	R/F(kN)	352	421	502	600	716
2	E/A(kN-m)	166	198	236	282	359
5	R/F(kN)	363	433	517	618	788
Bolt S	ize: X6pcs	M30	M30	M30	M30	M36

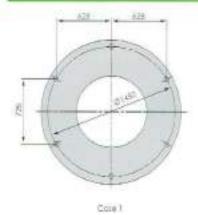


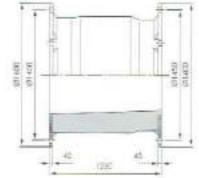


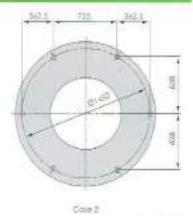
Weight: 1205kg

	1150H	F4	F3	F2	FT	FO
A.	E/A(kN-m)	217	259	309	369	441
.v.	R/F(kN)	414	494	590	705	842
	E/A(kN-m)	224	267	319	381	454
	R/F(kN)	426	509	608	726	867
2	E/A(kN-m)	230	275	328	392	468
	R/F(kN)	439	524	626	748	893
3	E/A(kN-m)	237	283	338	404	482
2	R/F(kN)	452	540	645	770	920
4	E/A(kN-m)	244	292	348	416	496
1	R/F(kN)	466	556	664	793	947
e :	E/A(kN-m)	252	300	359	428	546
5	R/F(kN)	480	573	684	817	1042
olt SI	ze: X6pcs	M30	M30	M36	M36	M36

1250H





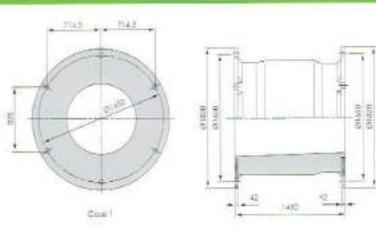


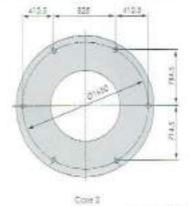
Neight 1650kg

	1250H	F4	F3	F2	F1	FO
	E/A[kN-m]	279	333	397	474	566
0 1 2 3 4	R/F(kN)	489	584	697	833	995
1	E/A[kN-m]	287	343	409	488	583
1	R/F(kN)	504	602	718	858	1024
0	E/A[kN-m]	29.6	353	421	503	600
4	R/F(kN)	519	620	740	884	1055
	E/A(kN-m)	304	363	434	518	618
	R/F(kN)	534	638	762	910	1087
11	E/A{kN-m}	314	374	447	534	637
4	R/F(kN)	550	657	785	937	1119
5	E/A(kN-m)	323	386	460	550	701
2	R/F(kN)	567	677	809	966	1231
Bolt S	ize: X6pcs	M30	M36	M36	M36	M36



1450H

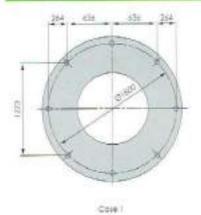


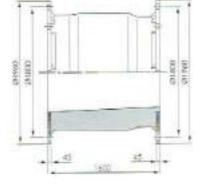


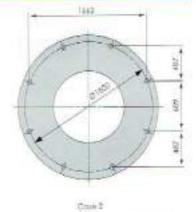
Weight 1350kg

CS	\$1450H	F4	F3	F2	F1	FO
	E/A(kN-m)	434	519	619	739	883
0	R/F(kN)	658	786	939	1121	1338
	E/A(kN-m)	.447	534	638	761	909
1	R/F(kN)	678	810	967	1155	1379
	E/A(kN-m)	461	550	657	784	936
2	R/F(kN)	698	834	996	1189	1420
	E/A(kN-m)	475	567	677	808	964
3	R/F(kN)	719	859	1026	1225	1463
2	E/A(kN-m)	489	584	697	832	993
4	R/F(kN)	741	885	1057	1262	1507
-	E/A(kN-m)	504	601	718	857	1093
5	R/F(kN)	763	911	1088	1299	1657
Bolt S	ize: X6pcs	M36	M36	M42	M42	M42

600H



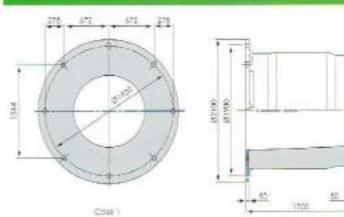




Weight 2Willia

CS	S1600H	F4	F3	F2	F1	FO
-	E/A(kN-m)	583	696	831	992	1185
0	R/F(kN)	802	957	1143	1365	1630
22	E/A(kN-m)	601	717	856	1022	1221
A:	R/F(kN)	826	986	1177	1406	1679
1	E/A(kN-m)	619	739	882	1053	1257
2	R/F(kN)	850	1015	1213	1448	1729
100	E/A(kN-m)	637	761	908	1084	1295
3	R/F(KN)	876	1046	1249	1491	1781
1	E/A[kN-m]	656	784	936	1117	1334
4	R/F(kN)	902	1077	1287	1536	1834
	E/A(kN-m)	676	807	964	1150	1467
5	R/F(kN)	929	1110	1325	1582	2018
Bolt S	Ize: X8pcs	M36	M36	M36	M42	M42





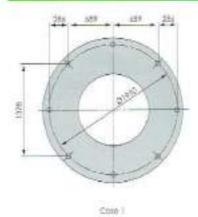


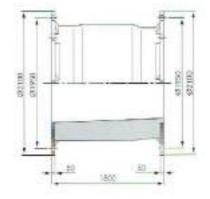
03100

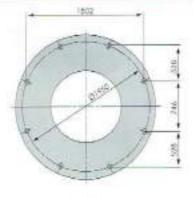
iveignt 3/30kg

	1700H	F4	F3	F2	FT	FO
~	E/A(kN-m)	699	835	997	1190	1421
U	R/F(kN)	905	1081	1290	1541	1840
	E/A(kN-m)	720	860	1027	1226	1463
1	R/F(kN)	932	1113	1329	1587	1895
	E/A(kN-m)	742	886	1057	1262	1507
2	R/F(kN)	960	1146	1369	1635	1952
3	E/A(kN-m)	764	912	1089	1300	1552
3	R/F(kN)	989	1181	1410	1684	2011
<u></u>	E/A(kN-m)	787	939	1122	1339	1599
4	R/F(kN)	1019	1216	1452	1734	2071
2	E/A[kN-m]	810	968	1155	1379	1759
5	R/F(kN)	1049	1253	1496	1786	2278
Bolt S	ize: X8pcs	M36	M36	M42	M42	M42

1800H







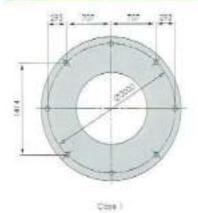
Cote 2

	1800H	F4	F3	F2	F1	FO
~	E/A(kN-m)	830	990	1183	1412	1686
0 1 2 3	R/F(kN)	1015	1212	1447	1728	2063
4	E/A(kN-m)	854	1020	1218	1454	1736
1	R/F(kN)	1045	1248	1490	1779	2125
2 1	E/A[kN-m]	880	1051	1255	1498	1789
	R/F(kN)	1076	1285	1535	1833	2189
-	E/A[kN-m]	906	1082	1292	1543	1842
8	R/F(kN)	1109	1324	1581	1888	2254
1	E/A[kN-m]	934	1115	1331	1589	1897
4	R/F(kN)	1142	1364	1628	1944	2322
	E/A[kN-m]	962	1148	1371	1637	2087
5	R/F(kN)	1176	1405	1677	2003	2554
Bolt S	ize: X8pcs	M42	M42	M42	M48	M48

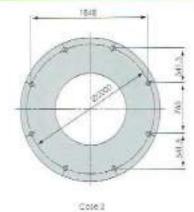
Weight: 4550kg

# CHICOR

#### 2000H



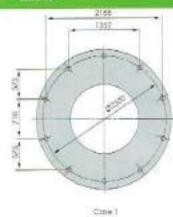




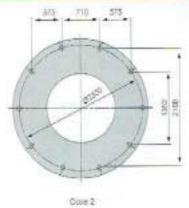
weight: 5565(g)

	2000H	F4	F3	F2	F1	FQ
	E/A(kN-m)	1137	1358	1621	1935	2311
D	R/F(kN)	1253	1496	1786	2133	2547
	E/A(kN-m)	1171	1398	1670	1994	2380
4	R/F(kN)	1290	1541	1840	2197	2623
-	E/A(kN-m)	1206	1440	1720	2053	2452
2	R/E(kN)	1329	1587	1895	2263	2702
-	E/A(kN-m)	1242	1483	1771	2115	2525
3	R/F(kN)	1369	1635	1952	2331	2783
24	E/A(kN-m)	1280	1528	1824	2178	2601
4	R/F(kN)	1410	1684	2010	2401	2867
140	E/A(kN-m)	1318	1574	1879	2244	2861
5	R/F(kN)	1452	1734	2071	2473	3153
Bolt S	ize: X8pcs	M48	M48	M48	M56	M56

2250H





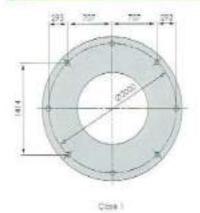


weight 748kg

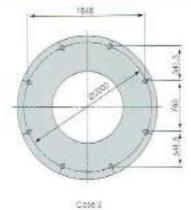
	2250H	F4	F3	F2	F1	FO
	E/A(kN-m)	1618	1931	2306	2753	3288
0	R/F(kN)	1586	1893	2261	2700	3224
Sat	E/A(kN-m)	1666	1989	2375	2836	3386
10	R/F(kN)	1633	1950	2329	2781	3320
~	E/A(kN-m)	1716	2049	2446	2921	3488
2	R/F(kN)	1682	2009	2399	2864	3420
	E/A(kN-m)	1768	2110	2520	3009	3593
3	R/F(kN)	1733	2069	2470	2950	3523
	E/A(kN-m)	1821	2174	2595	3099	3700
4	R/F(kN)	1785	2131	2545	3038	3628
	E/A(kN-m)	1875	2239	2673	3192	4070
5	R/F(kN)	1838	2195	2621	3130	3991
Bait Si	ze: X10ocs	M48	M48	M48	M56	M56



#### 2000H







walgriti 526040

	2000H	F4	F3	F2	F1	FO
14	E/A(kN-m)	1137	1358	1621	1935	2311
,U	R/F(kN)	1253	1496	1786	2133	2547
, E/A(kN-m)	1171	1398	1670	1994	2380	
1	R/F(kN)	1290	1541	1840	2197	2623
-	E/A[kN-m]	1206	1440	1720	2053	2452
2	R/F(kN)	1329	1587	1895	2263	2702
~	E/A[kN-m]	1242	1483	1771	2115	2525
3	R/F(kN)	1369	1635	1952	2331	2783
	E/A[kN-m]	1280	1528	1824	2178	2601
4	R/F(kN)	1410	1684	2010	2401	2867
-	E/A[kN-m]	1318	1574	1879	2244	2861
5	R/F(kN)	1452	1734	2071	2473	3153
Bolt S	ize: X8pcs	M48	M48	M48	M56	M56



CELL TYPE FENDER





BATANGAS PORT





# HICOR V-TYPE FENDER



### V-SHAPED FENDER

### V-type fender

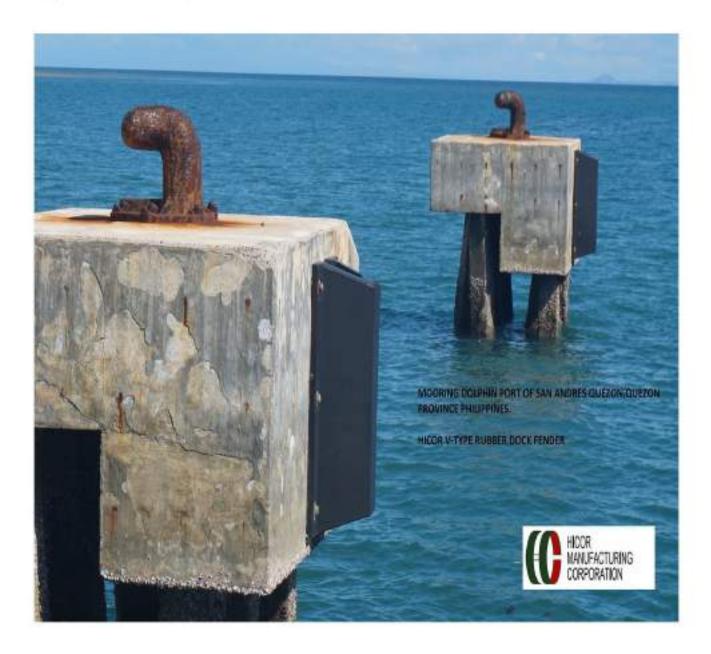
A conventional cylindrical type fender absorbed energy through compressive deformation, while this V-type fender materialized a revolutionary improved energy absorption efficiency by adding the compressive deformation to bucking deformation.

Once again, the introduction of a stationary system with anchor bolts improved the durability remarkably.

This fender is used most widely in the world harbors as "multipurpose type" fender.

### Features

- 1) Excellent energy absorption efficiency
- 2) Excellent durability and stability





### **V FENDER PERFORMANCE** Fender Performance At 45% Design Deflection (Rated Performance Data)

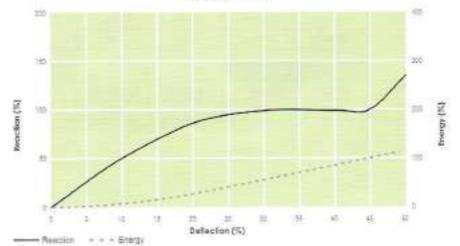
_	1	ri -	1	/2	10 34	(3	)	/4	1.000	
lize	Reaction Force	Energy Absorption	Reaction Force	Energy Absorption	Reaction Force	Energy Absorption	Reaction Force	Energy Absorption	LENGTH Up to:	52e
	[tent]	(tent-m)	(tont)	(m-fnot)	Itonti	(tani-m)	(tor?)	(tonf-m)	mm	
150	12.8	0.641	11,3	0.563	8.44	0.422	5.63	0.281	3500	1.50
200	17.1	1,14	15.0	1.00	11.3	0,750	7.50	0.500	3500	200
250	21.4	1,78	78,8	1.56	14.1	1,17	9.38	0.781	3500	250
300	25.7	2.57	22.5	2.25	16.9	1.69	11.3	1.13	3500	300
400	34.2	4.55	30:0	4.00	22.5	3.00	15.0	2.00	3500	400
500	42.8	7.13	37.5	6.25	28.1	4,69	18.6	3.13	3000	500
600	51.3	10.3	45.0	9.00	33.8	6.75	22.5	4.50	3000	600
800	68.4	18.2	60.0	T6.0	45.0	12.0	30.0	8.00	3000	800
000	85.5	28.5	75.0	25.0	56.3	18.6	37.5	12.5	3000	1000
	1	×1		v2		/3	V4			-
5ize	Recotion Force	Energy Abtorphion	Reaction Force	Energy Absorption	Reaction Force	Briergy Absorption	Reaction Force	Shergy Abscription	LENGTH Up to	Size
	(kN)	(kN-m)	(kN)	(kN-m)	(kN)	(kN-m)	(RN)	(kN-m)	mm	
150	126.0	6.29	111	5.52	82.8	4.14	55.2	2.76	3500	150
200	168	11.2	147	9.81	111	7.35	73.5	4.90	3500	200
250	210	17.5	184	15.3	138	11.5	92.0	7.66	3500	250
300	252	25.2	221	22,1	166	16.6	111	11.1	3500	300
400	335	44.7	294	39.2	221	29.4	147	19.6	3500	400
500	420	69.9	368	61.3	276	46.0	184	30.7	3000	500
600	503	101	441	88.3	331	66.2	221	44.1	3000	600
900	67	178	588	157	441	118	294	78.5	3000	800

Performance Per Meter Length with 45% Deflection \* Specification will be changed without prior notice. \* Special Rubber Grade can be available due to design condition.

\*PERFORMANCE TOLERANCE ± 10%

Del(%)	R/F	E/A
0%	0%	0%
10%	50%	7%
20%	86%	28%
30%	99%	56%
40%	99%	85%
45%	100%	100%
50%	135%	118%

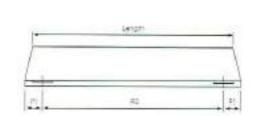


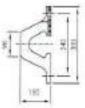




V150H





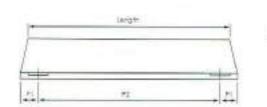


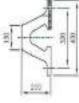
Length	P1	P2	Weight	No. Bolt	Bolt Size
1000L	87.5mm	900mm	34kg	4	
1500L	87.5mm	700mm	50kg	6	
2000L	92,5mm	630mm	66kg	8	M20
2500L	87,5mm	800mm	82kg	8	M24
30001	87.5mm	725mm	98kg	10	
35001	87.5mm	680mm	114kg	10	

	V1		V2	V3		V.4	
R/F(kN)	E/A(kN-m)	R/FjkN)	E/A(kN-m)	R/F[kN]	E/A(kN-m)	R/F(ktvl)	E/A(kN-m)
126	6.29	111	5.52	82.8	4.14	55,2	2.76

V200H







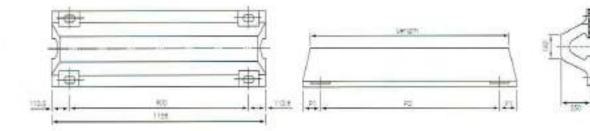
100mm	900mm	2012210		
	and a second sec	60kg	4	
100mm	700mm	89kg	6	
105mm	630mm	117kg	8	M20
100mm	800mm	146kg	8	M24
100mm	725mm	175kg	10	
100mm	680mm	203kg	10	
	100mm	100mm 725mm	100mm 725mm 175kg	100mm 725mm 175kg 10

	V1		V2	V3		V4	
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F(kN)	E/A/kN-mi
168	11.2	147	9.81	111	7.35	73:5	4.90



88

### V250H

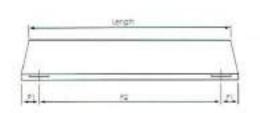


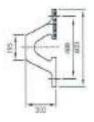
Length	P1	P2	Weight	No. Bolt	Bolt Size
1000L	112.5mm	900mm)	87kg	4	
1500L	112.5mm	700mm	1:28kg	6	
2000L	117.5mm	630mm	169kg	8	M20
25001	112.5mm	800mm	210kg	8	M24
3000L	112.5mm	725mm	250kg	10	
35001	112.5mm	680mm	291kg	10	

¥1		V2		V3		V4	
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F[kN]	E/A[kN-m]	R/F(kN)	E/A(kN-m)
210	17.5	184	15.3	138	11.5	92.0	7.66

### V300H



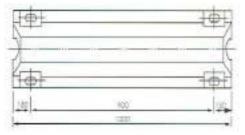


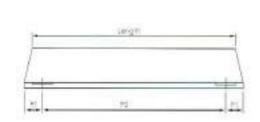


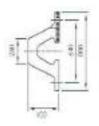
	Length	Pl	P2	Weight	No. Bolt	Bolt Size	
	1000L	125mm	900mm	133kg	4		
	1500L	125mm	700mm	194kg	6		
	2000L	130mm	630mm	254kg	8	M20	
	2500L	125mm	800mm	316kg	В	M30	
	3000L	125mm	725mm	377kg	10		
	3500L	125mm	680mm	438kg	10		
	/1	3	V2		/3	-23	V4
R/F(kN)	E/A(kN-m)	R/F[kN]	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F[kN]	E/A(kN-m)
252	25.2	221	22.1	166	16.6	111	11.1



V400H



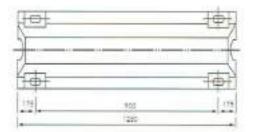




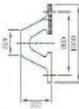
Length	Pl	P2	Weight	No, Bolt	Bolt Size
1000L	150mm	900mm	245kg	4	
1500L	150mm	700mm	354kg	ó	
20001.	155mm	630mm	463kg	8	M24
2500L	15Dmm	800mm	57.5kg	8	M36
30000	150mm	725mm	684kg	10	<ul> <li>PD-32458</li> </ul>
3500L	150mm	680mm	793kg	10	

	V1	V2		va.		V4	
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F[KN]	E/A(kN-m)	R/F(kN)	E/A(kN-m)
335	44.7	294	39.2	221	29.4	147	19,6

### V500H





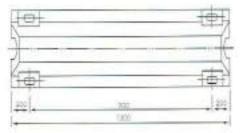


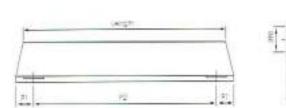
Length	PT	P2	weight	No. Boit	Bolt \$ize
1000L	175mm	900mm	364kg	4	
1.500L	175mm	700mm	523kg	6	
2000L	180mm	630mm	682kg	8	M27
25001	175mm	800mm	844kg	8	N36
3000L	175mm	725mm	1,003kg	10	COCHTR
3500L	175mm	680mm	1,1.59kg	10	1

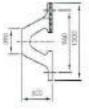
	V1		V2		V3	()	74
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A[kN-m]	R/F(kN)	E/A[kN-m]	R/F(kN)	E/A(kN-m
420	69.9	368	61.3	276	46.0	184	30.7



### V600H





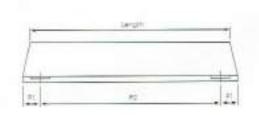


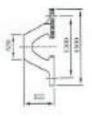
Length	P1	P2	Weight	No, Bolt	Bolf Size
10001.	200mm	900mm	526kg	4	
15001	200mm	700mm	750kg	6	M30
20001	205mm	630mm	945kg	8	-
2500L	200mm	800mm	1,204kg	8	M42
30000	200mm	725mm	1.428kg	10	B

1	V1	V2		V3		V4	
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)
503	101	441	88.3	331	65.2	221	44.1

### V800H





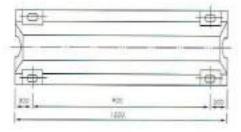


Length	P1	P2	Weight	No. Bolt	Bolt Size
1000L	250mm	900mm	890kg	.4	
15000	250mm	700mm	1.255kg	é	M30
20001.	255mm	630mm	1.620kg	8	-
2,5000	250mm	800mm	1,993kg	8	M48
30001	250mm	725mm	2.358kg	10	

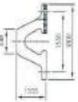
	Vš	¥2			/3	V4	
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)
671	178	588	157	447	118	294	78.5



### V1000H







Length	P1	P2	Weight	No. Bolt	Bolt Size
1000L	300mm	900mm	1,389kg	4	
1500L	300mm	700mm	1,935kg	6	M36
2000L	305mm	630mm	2.482kg	8	-
2500L	300mm	800mm	3.041kg	8	M45
3000L	300mm	725mm	3.588kg	10	

	V1		V2	1	εv		V4
R/F(kN)	E/A(kN-m)	R/F(kN)	E/A(kN-m)	R/F kN}	E/A(kN-m)	R/F(kN)	E/A/kN-m)
838	279	735	245	552	184	368	123





# OTHER TYPES OF HICOR FENDER M-TYPE PI-TYPE

CYLINDRICAL HYPER OMEGA SQUARE TYPE D-TYPE CORNER FENDER





PHILEX MINING CORP. PORO POINT LA UNION

HICOR PI-TYPE RUBBER DOCK FENDER WITH PANEL BOARD

# HICOR PI-TYPE FENDER

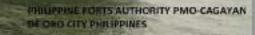




PPA-PMO TAGBILARAN, BOHOL CYLINDRICAL TYPE RUBBER DOCK FENDER

20

# HICOR CYLINDRICAL-TYPE FENDER

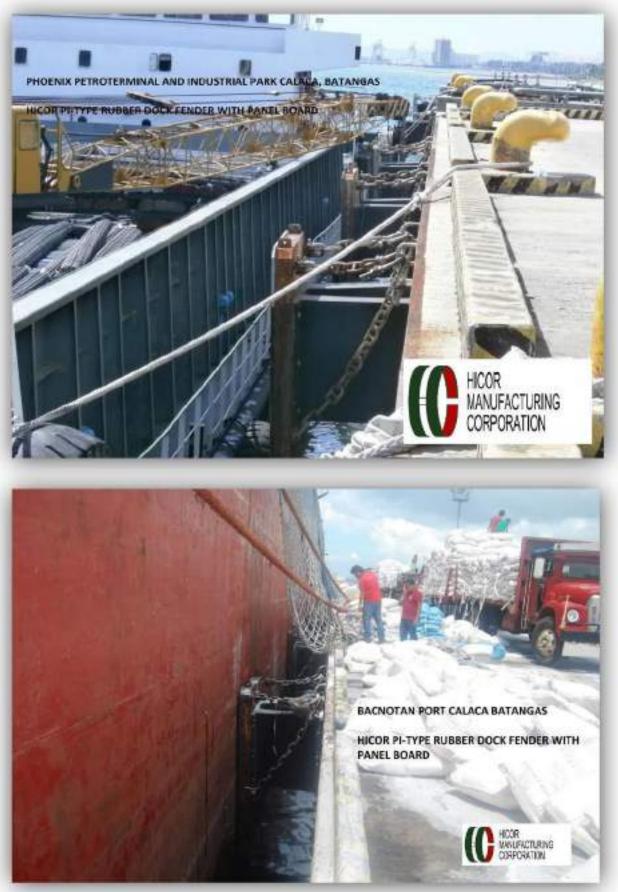


HICOR MANUFACTURING CORPORATION

HICOR M TYPE RUBBER DOCK FENDER

# HICOR M-TYPE FENDER





# HICOR PI-TYPE FENDER





# HICOR PI-TYPE FENDER



ACTUAL COMPRESSION TEST AT HICOR PLANT



### **HICOR D-TYPE FENDER**

HICOR D-type fender provide an excellent barrier against damage from all sizes and shapes of vessels. They provide easy installation because of its flat back feature. Non-standard sizes and customer specific versions can also be produced with short lead times.

### MAIN APPLICATION

HICOR D-type fenders suites a wide variety of general purpose application.

- Jetties and Wharves
- Workboats and service crafts
- Mooring pontoon protection
- Inland waterways
- General Purpose application.







PORT OF TAGBILARAN, PPA BOHOL HICOR D-TYPE FENDERS



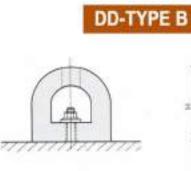
# **D-TYPE FENDERS**

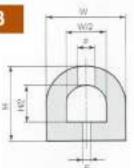
# **HICOR D-TYPE FENDERS**

THIS TYPE OF RUBBER FENDER IS SUITABLE FOR WHARVES AND QUAYS WHERE IT ACTS AS A GREAT PROTECTIVE MEDIUM FOR VESSEL BERTHINGS. THE FLAT BACK OF THIS TYPE OF FENDER FACILITATES EASY INSTALLATION ON VARIOUS SURFACES.



DD-TYPE A





### TYPE A

IIIEA					Note: Perfor	mance refers t	o the state at 5	0% deflection
Item	150H	200H	250H	300H	350H	400H	500H	600H
н	150	200	250	300	350	400	500	600
W	150	200	250	300	350	400	500	600
В	30	35	45	55	65	75	95	120
C (Ø)	27	30	33	36	40	45	50	55
Bolt size	W 7/8	W 1	W 1 1/8	W 1 1/4	W 1 3/8	W 1 1/2	W 1 3/4	W 2
Bolt pitch	400 - 470	400 - 470	390 - 470	530 - 700	530 - 700	520 - 600	510 - 640	500 - 750
Reaction/m (ton)	14.3	19.0	23.8	28.5	33.5	38.0	47.9	57.1
Energy/m (ton-m)	0.357	0.631	0.989	1.42	1.91	2.52	3.95	5.67

Item	150H	200H	250H	300H	350H	400H	500H	600H
н	150	200	250	300	350	400	500	600
w	150	200	250	300	350	400	500	600
E (Ø)	27	30	33	36	40	45	50	55
F (Ø)	60	65	75	80	85	95	105	115
Bolt size	W 7/8	W 1	W 1 1/8	W 1 1/4	W 1 3/8	W 1 1/2	W 1 3/4	W 2
Bolt pitch	400 - 470	400 - 470	390 - 470	530 - 700	530 - 700	520 - 600	510 - 640	500 - 750
Reaction/m (ton)	7.21	9.61	12.0	14.4	16.8	19.2	24.0	28.8
Energy/m (ton-m)	0.206	0.364	0.570	0.819	1.08	1.45	2.27	3.26

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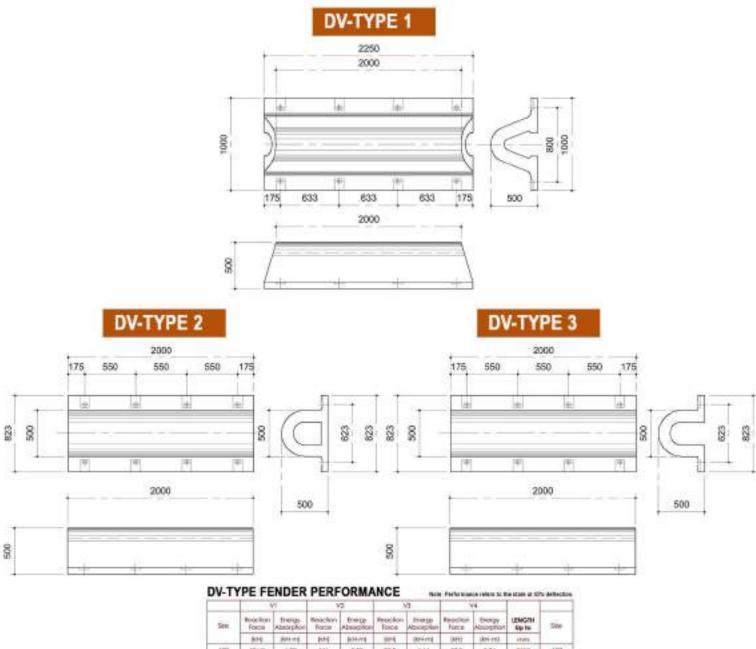






# **D-TYPE FENDERS**

# **HICOR DV-TYPE FENDERS**



							1.1			
See.	Rodelton Forpa	broup Absorption	Reaction Rates	brenge Absorption	Resident Race	Therap Absolption	Reporter Force	- Energy Absorption	LENGTH Up to	500
	814	japa-mg	PMI ·	\$04400	(874	0074-001	Dett:	AN-110	1000	·
180	CIAII	6.29	111	5.52	82.8	4.14		3.76	3990	490
200	168	11.2	147	10.0	111	7.35	. 73.5	-4.90	1000	231
290	210	17.5	Tibi	15.5	120	115	910	7.66	39(0)	290
300	282	25.2	721	(数1)	165	16.6	111	11.3	2990	300
400	335	44.7	294	. 312	221	25.4	147	12.6	3000	430
500	-420	62.9	268	61.3	176	40	154	30.7	3000	(00)
400	808	101	441	18.5	101	5.66	221	-44.1	3000	400
600	421	170	200	157	441	110	294	38.6	3000	100
1000	838	279	738	345	8.62	184	348	123	1.000	1000

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WE BUILD PRODUCTS THAT BUILD CONFIDENCE

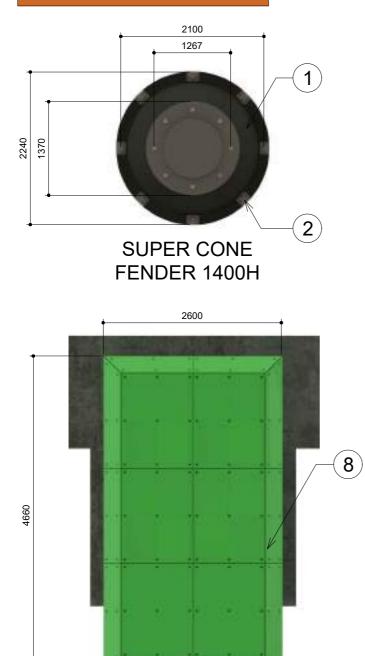




# **SUPER CONE FENDERS**

# HICOR SUPER CONE TYPE FENDERS

H-SCN- 1400H FENDERS



### **FRONT PANEL**

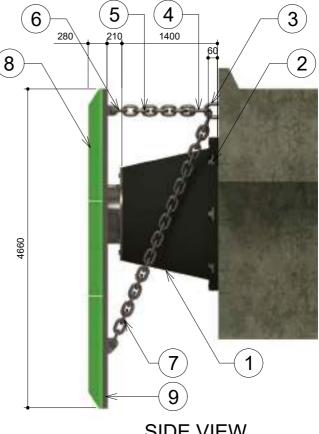
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### SUPER CONE FENDER 1400H WITH 4660mm(H)X2600mm(W) FRONT PANEL

MATERI	AL SCHEDULE	
<b>БРАН</b> КК	JUSCHO-DOM	VAREAL
· · ·	C-SNU RUNDER (1996-1996)	Kalin-Achife (edd), Higgle X() (-O
2	AND DE ROUT, MARKER NEU DE RES	\$\$7.0(5\$19.72 <b>\$</b> 7)
1	1 AMONTH AMARA	\$\$7.0(3519.2287)
`	10.8 YOUNTER LIVE &	507290 0.54 105010 650 9 C10 <sub>6</sub> 967 1
5	0.9500 C14.9 1.54175	MERITOL DRIVERSHIP STREAM 1
- 4 - <sup>1</sup>	N 8001 N 917	MC89000103010309770gabba
- <u>,</u> '	VERSITE COMPLETE AD	ABC4911001 DRPED GREV S BY 2002 http://www.com/
.1	LINNAPENTE AD FONTANELINAPENTE	UPDOTATION COUCH GALLY
	SILL MARKEPANEL	SV56004, ASTMARS W/ MARINE STORY PA NIED COLLEGATION

PERFORMANC	E TABLE		TOLERANCE = ±10
MAR:	DEFLECTION	REACTION FORCE (FOR	ENERGY RESOLVED TO ME ME
HISCH L400H	72%	1790.20	L411.50



SIDE VIEW

WE BUILD PRODUCTS THAT BUILD CONFIDENCE

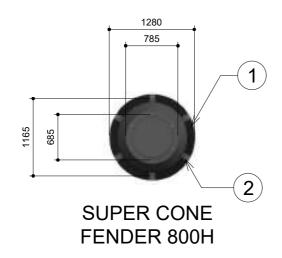




# **SUPER CONE FENDERS**

# **HICOR SUPER CONE TYPE FENDERS**

### H-SCN- 800H FENDERS



SUPER CONE FENDER 800H WITH 4000mm(H)X1500mm(W) FRONT PANEL

MATERIAL SCHEDULE					
KIND	5050-904 CK	MATL: AL			
:	CONE (CNEE & SOCKIM, P)	A TORAL HIGH GRADE PUBBLIC ADDING			
2	ANCHOR SOLF WARSER & VESTVE VISI	55K00[451 V A240			
1	J ANCHOR 25NTMX	55305[451 V As#0			
-	40.05161.01X	SSCHOLADED INSDIGATE SUBJECT			
	1. 99D 9 CE416 123	NEOROPOLI DI VINDI GALVINIQUEZI DI			
с. –	"HACKLE 112	NEOROPOID APPECIALS STRUMS IN			
1	AVE GHE CHAINE IN	NEOROPOID APPECIALS STRUMS IN			
.1	CHWM /LAVID FAD FLONE PANEL/ROWETTIK	OPMERAL FAD COLOF GALLY			
ч	MILLE FORME VANSU	ANTAICE ANTA A 66 MARINE STOT			

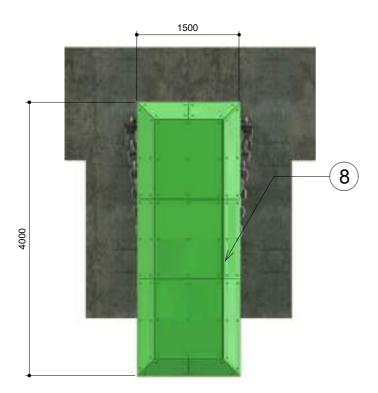
PERFORMANCE TABLE						
K3504	DEFLECTION .	REACT ON FORCE (Kn)	ENERGY ASSORETION (KILME			
HISCN XUOH	72%	:42 Ju	2:4 40			

120

280

6

800



FRONT PANEL

# HICOR MANUFACTURING CORPORATION

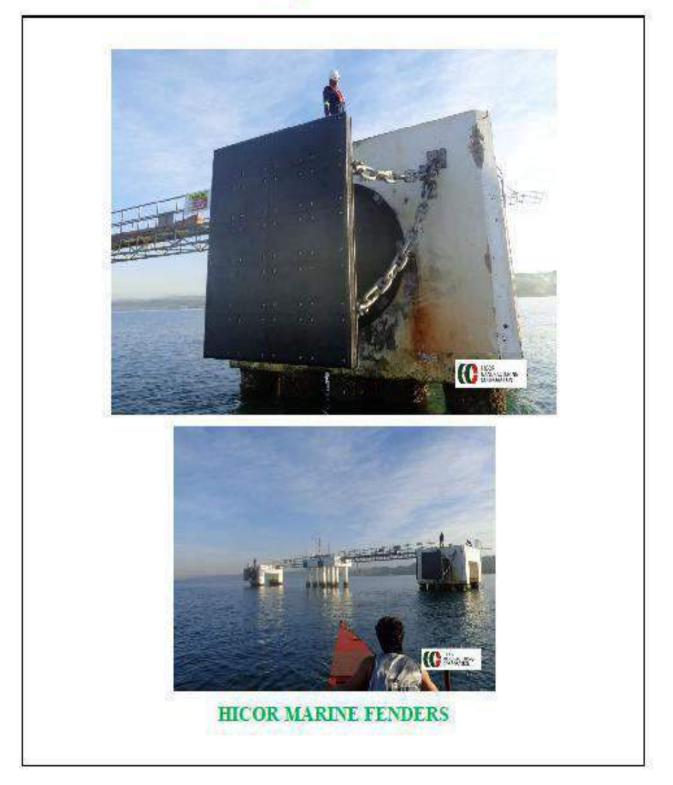
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4













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"WE BUILD PRODUCTS THAT BUILDS CONFIDENCE"